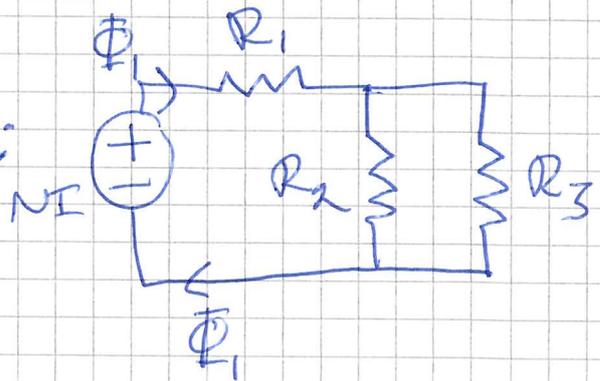


# EENISS tentamen 20/8 2025

## Kortfattade lösningar

① a) Beräkningsschema:



$$\begin{cases} A_1 = A_2 = A_3 \equiv A \\ \mu_1 = \mu_2 = \mu_3 = \mu_0 \mu_r \\ l_1 = l_3 = 3l_2 \end{cases}$$

$R_2$  &  $R_3$  är parallellkopplade.

$R_1$  i serie med  $R_2 // R_3$

$$\Rightarrow R_1 = R_3 = 3R_2$$

$$R_{tot} = R_1 + \frac{R_2 R_3}{R_2 + R_3} = R_2 \left( 3 + \frac{3}{4} \right)$$

$$R_2 = \frac{l_2}{\mu_0 \mu_r A} = \frac{5 \cdot 10^{-2}}{4\pi \cdot 10^7 \cdot 2 \cdot 10^3 \cdot 3 \cdot 10^{-4}} \approx 6,63146 \text{ } \Omega/\text{H}$$

$$\Rightarrow R_{tot} \approx 2,486796 \cdot 10^5 \text{ } \Omega/\text{H}$$

$$\begin{cases} NI = R_{tot} \cdot \Phi_1 \\ \Phi_1 = B_1 A \end{cases} \Rightarrow I = \frac{R_{tot} \cdot B_1 A}{N} \approx \underline{\underline{0,23 \text{ ampere}}}$$

b) Gauss lag för magnetfält

2) a)  $\vec{\Pi} = m \times \vec{B}$ ,  $m = NIA \cdot \vec{m}$

$\Rightarrow \vec{\Pi} = NIA \cdot m \times \vec{B}$  med  $m = -\sin\varphi \hat{x} + \cos\varphi \hat{y}$   
 $\vec{B} = B_x \hat{x} + B_y \hat{y}$

$\left. \begin{aligned} \hat{x} \times \hat{x} = \hat{y} \times \hat{y} = 0 \\ \hat{x} \times \hat{y} = \hat{z}, \hat{y} \times \hat{x} = -\hat{z} \end{aligned} \right\} \Rightarrow m \times \vec{B} = (-\sin\varphi B_y - \cos\varphi B_x) \hat{z}$

$\therefore \vec{\Pi} = NIA \cdot (\sin\varphi B_y + \cos\varphi B_x) \cdot (-\hat{z})$

$\varphi = 30^\circ \Rightarrow \sin 30^\circ = 0,5 \quad \& \quad \cos 30^\circ = \frac{\sqrt{3}}{2} \approx 0,866$

$\Rightarrow \vec{\Pi} = 10 \cdot 1,5 \cdot 0,12^2 \cdot (0,5 \cdot 0,4 + 0,866 \cdot 0,11) \cdot (-\hat{z})$   
 $\approx -0,0619 \hat{z} \text{ Nm}$

$\therefore$  Vridmomentet  $\vec{\Pi} \approx \underline{\underline{-0,0619 \text{ Nm}}}$ , riktat  $\otimes$

b)  $\vec{B}$  beror här ej av rumsposition  $\Rightarrow \Phi = \vec{B} \cdot \vec{A}$   
genom slingan

$\vec{B} = B_x \cos\omega t \hat{x} + B_y \sin\omega t \hat{y}$   
 $\vec{A} = A \cdot \hat{y}$

$\Rightarrow \boxed{\Phi = B_y \cdot A \cdot \sin\omega t}$

$\hat{x} \cdot \hat{y} = 0$   
 $\hat{y} \cdot \hat{y} = 1$

endast  $B_y$ 's  $\hat{y}$ -komponent bidrar

$U_{\text{ind}} = -N \frac{d\Phi}{dt} = -NB_y A \omega \cos\omega t$

$t = 2,5 \cdot 10^{-5} \text{ s} \Rightarrow |U_{\text{ind}}| = 5 \cdot 200 \cdot \pi \cdot 0,04^2 \cdot 10^5 \cdot \cos(10^5 \cdot 2,5 \cdot 10^{-5}) \approx \underline{\underline{4,0 \text{ V}}}$

3

Elektriska flödet genom en yta:

$$\Phi_e = \int_{\text{yta}} \mathbb{D} \cdot d\mathbf{A} = \epsilon_0 \int_{\text{yta}} \mathbb{E} \cdot \mathbf{n} \, dA$$

dar  $\mathbf{n}$  = normalvektor till ytan,  
riktas ut från ytan om ytan  
del av slutets område.

Uppgiften:  $\mathbb{E}$  riktar i  $+\hat{x} \Rightarrow$  passerar  
genom kubens sidor i  $yz$ -planet.

Vid  $x=0$  är  $\mathbf{n} = -\hat{x}$ , vid  $x=0,01\text{m}$  är  
 $\mathbf{n} = +\hat{x}$ .

$\mathbb{E}$  oberoende av  $y$  &  $z \Rightarrow$  integration över  
en kubida ger  $\mathbb{E} \cdot \mathbf{n} \cdot \text{arean av sidan}$ .

$\Rightarrow$  Totala flödet genom kuben blir:

$$\Phi_{e,\text{tot}} = \Phi_e(x=0) + \Phi_e(x=0,01) =$$

$$= \left[ 25000 \cdot (1+2 \cdot 0) \cdot (-1) + 25000 \cdot (1+2 \cdot 0,01) \cdot (+1) \right] \cdot \epsilon_0 \cdot 0,01^2$$

$\uparrow \hat{x} \cdot (-\hat{x})$                        $\hat{x} \cdot \hat{x}$

$\uparrow$  arean hos en kubsida

$$\approx 4,43 \cdot 10^{-13} \text{ coulomb}$$

Gauss lag för el. fält:  $Q_{\text{inre}} = \Phi_{e,\text{tot}} \approx \underline{\underline{4,4 \cdot 10^{-13} \text{ C}}}$   
(positiv laddning)

4a)  $N_f = 440 \text{ V}$        $V_T = 350 \text{ V}$        $T_L = B \cdot \omega_r = 0.6 \omega_r$

i) varvtal?

$$V_T = R_a \dot{i}_a + \lambda \omega_r$$

$$V_T = R_a \frac{B}{\lambda} \omega_r + \lambda \omega_r$$

$$\left\{ \begin{array}{l} T_e = \lambda \dot{i}_a = T_L = B \omega_r \\ \Rightarrow \dot{i}_a = \frac{B \omega_r}{\lambda} \end{array} \right.$$

$\lambda$ ?

$$V_f = 440, R_f = 200$$

$$I_f = \frac{440}{200} = 2.2 \text{ A}$$

$$\Rightarrow \lambda = 1.63 \text{ Wb}$$

$$V_T = \omega_r \left( \frac{R_a B}{\lambda} + \lambda \right) \Rightarrow \omega_r = \frac{V_T}{\frac{R_a B}{\lambda} + \lambda} = \frac{350}{\frac{0.22 \cdot 0.6}{1.63} + 1.63} = 204.561 \text{ rad/s}$$

$$\underline{\underline{n_r = \omega_r \cdot \frac{30}{\pi} = 1953.4 \text{ rpm}}}$$

ii)  $\dot{i}_a$ ?

$$\underline{\underline{\dot{i}_a = \frac{B \cdot \omega_r}{\lambda} = \frac{0.6 \cdot 204.561}{1.63} = 75.3 \text{ A}}}$$

ok < märkström 127 A

iii) motenk?

$$\underline{\underline{e_a = \lambda \omega_r = 1.63 \cdot 204.561 = 333.4 \text{ V}}}$$

iv)  $\underline{\underline{P_{cu,f} = R_f \overset{\text{se ovan}}{\hat{i}_f^2} = 200 \cdot 2.2^2 = 968 \text{ W}}}$

v)  $\underline{\underline{P_{mek} = \omega_r \cdot T_e = \omega_r \cdot \lambda \cdot \dot{i}_a = 204.561 \cdot 1.63 \cdot 75.3 = 25107.61 \dots \text{ W}}}$   
 $\approx \underline{\underline{25.1 \text{ kW}}}$

4b)

$$V_T = \text{märkspänning} = 440 \text{ V}$$

$$\hat{i}_a = \text{märkström} = 127 \text{ A}$$

$$T_L = B \cdot \omega_r = 0.6 \cdot \omega_r \text{ Nm}$$

$$V_f, \hat{i}_a, \lambda = ?$$

$$\textcircled{1} \quad V_T = R_a \hat{i}_a + \lambda \omega_r \quad T_e = \lambda \hat{i}_a = T_L = B \cdot \omega_r \Rightarrow \omega_r = \frac{\hat{i}_a \lambda}{B} \quad \textcircled{2}$$

② i ①

$$V_T = R_a \hat{i}_a + \lambda \frac{\hat{i}_a \lambda}{B}$$

$$\lambda^2 \frac{\hat{i}_a}{B} = V_T - R_a \hat{i}_a \Rightarrow \lambda = \pm \sqrt{\frac{V_T - R_a \hat{i}_a}{\hat{i}_a / B}} = \sqrt{\frac{440 - 0.22 \cdot 127}{127 / 0.6}} = 1.395 \dots \text{ Wb}$$

$$\lambda \text{ i } \textcircled{2} \Rightarrow \omega_r = \frac{\hat{i}_a \cdot \lambda}{B} = \frac{127 \cdot 1.395}{0.6} = 295.275 \text{ rad/s}$$

$$\underline{\underline{n_r = \omega_r \cdot \frac{30}{\pi} = 2819.7 \text{ rpm}}}$$

$$\lambda = k_a \cdot \hat{i}_f$$

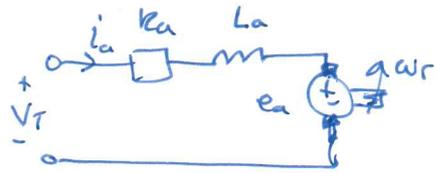
vid 2.2 A är  $\lambda = 1.63$ 

$$\Rightarrow k_a = \frac{\lambda}{\hat{i}_f} = \frac{1.63}{2.2} = 0.74091 \text{ Wb/A}$$

$$\underline{\underline{\hat{i}_f = \frac{\lambda}{k_a} = \frac{1.395}{0.74091} = 1.883 \text{ A}}}$$

4c)

ankarbrettens ekvivalenta krettschema

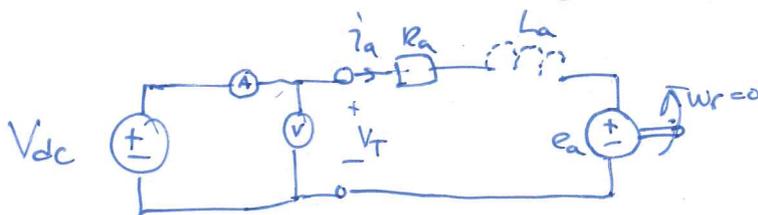


$$V_T = R_a i_a + L_a \frac{di_a}{dt} + \underbrace{2\omega r}_{e_a}$$

För att mäta  $R_a$  bör förutsättningarna vara sådana att varken  $L_a$  eller  $e_a$  inverkar. Det gör de ej om

- $V_T = \text{dc-spänning i stationärtillstånd} \Rightarrow \frac{di_a}{dt} = 0$
- $e_a = 0$ , det sker om  $V_f = 0 \Rightarrow \dot{\varphi} = 0 \Rightarrow A = 0$   
genom att inte magnetisera maskinen. Låt fältspänningen vara noll, vilket ger noll fältström och noll länkat flöde.  
Då utvecklas inget vridmoment ( $T_e = 2 \cdot i_a = 0 \cdot i_a = 0$ ) och rotorn kommer inte att accelerera.  
Varvtalet förblir noll och ( $e_a = 2 \cdot \omega r = 0 \cdot 0 = 0$ .)

Så läss på en dc-spänning som ger en ankarström nära mätstäm



- mät ankarström (A) och ankar spänning (V)

$$R_a = \frac{V_T}{i_a}$$

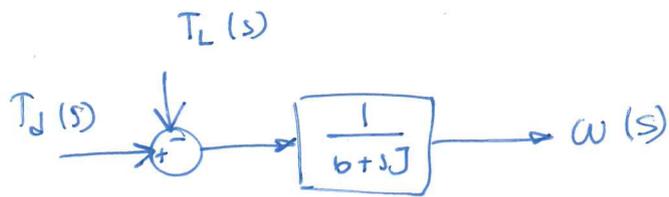
För att mäta  $L_a$  behöver även här  $e_a = 0$  så  $\dot{\varphi} = 0$ ,  $V_f = 0$ .

Samma uppställning som ovan men byt ut dc-spänningskällan mot en AC-spänningskälla med kärn fix frekvens  $f_s = V_{ac}$

Mät  $V_{T,rms}$ ,  $i_{a,rms}$   $|Z| = \frac{V_{T,rms}}{i_{a,rms}} = \sqrt{R_a^2 + \omega^2 L_a^2}$

där  $\omega = 2\pi f_s$ , lös ut  $L_a = \sqrt{\frac{\left(\frac{V_{T,rms}}{i_{a,rms}}\right)^2 - R_a^2}{(2\pi f_s)^2}}$

5a)



nedan härledning behöver ej redovisas

$$J \frac{dw(t)}{dt} = T_d(t) - b\omega(t) - T_L(t)$$

↓  $\mathcal{L}$

$$J s \omega(s) = T_d(s) - b \omega(s) - T_L(s)$$

$$T_d(s) - T_L(s) = J s \omega(s) + b \omega(s) = \omega(s) (J s + b)$$

$$\omega(s) = \left[ T_d(s) - T_L(s) \right] \cdot \left( \frac{1}{b + sJ} \right)$$

5b)

R, L i serie

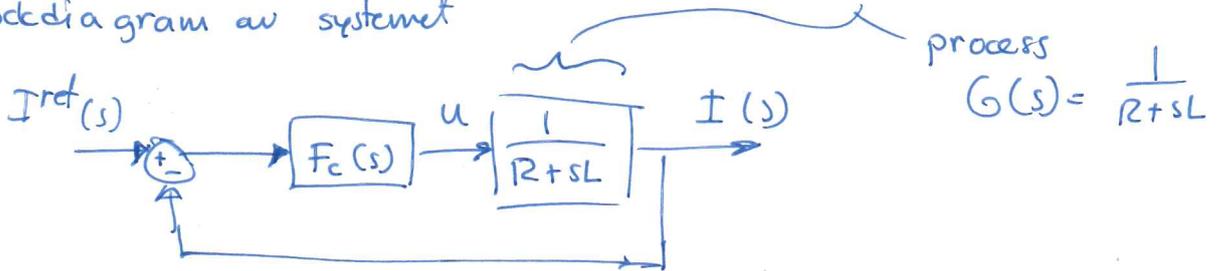
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$$i) \quad u = Ri + L \frac{di}{dt} \xrightarrow{\mathcal{L}} U(s) = R I(s) + L s I(s) = I(s) \cdot (R + sL)$$

- ström regulator  $F_c(s)$ 

$$I(s) = U(s) \cdot \left( \frac{1}{R + sL} \right)$$

- blockdiagram av systemet



- överföringsfunktion för det slutna systemet

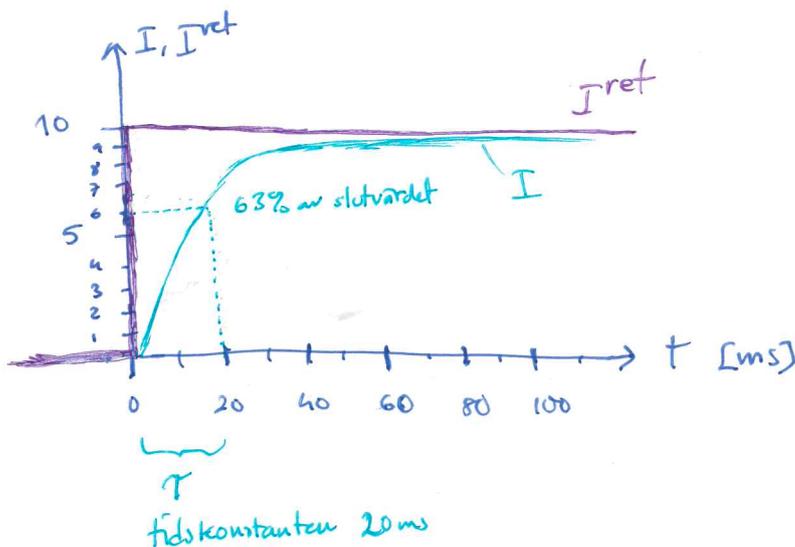
$$H(s) = \frac{I(s)}{I_{ref}(s)} = \frac{F_c(s) \cdot G(s)}{1 + F_c(s) \cdot G(s)} = \left. \begin{array}{l} \text{1:a ordns} \\ \text{system} \\ \Rightarrow \text{ingen} \\ \text{översväng} \end{array} \right\} = \frac{\alpha}{s + \alpha} = \frac{\alpha/s}{1 + \alpha/s}$$

$$\Rightarrow F_c(s) \cdot G(s) = \frac{\alpha}{s} \Rightarrow F_c(s) = G^{-1}(s) \cdot \frac{\alpha}{s} = (R + sL) \cdot \frac{\alpha}{s}$$

$$\Rightarrow F_c(s) = \underbrace{L \alpha}_{k_p} + \underbrace{\frac{R \alpha}{s}}_{k_i}$$

ii)

$$\tau = 20 \text{ ms} \quad I_{ref} = 10 \text{ A}$$



6a)  $D = f(I_d, I_o)$  ?

$$V_{L\text{ave}} = 0$$

$$V_{L\text{ave}} = \frac{1}{T} \int_0^T V_L(t) dt = 0$$

$$= \frac{1}{T} \int_0^{DT} V_L(t) dt + \frac{1}{T} \int_{DT}^T V_L(t) dt =$$

$$= \frac{1}{T} \int_0^{DT} (V_d - V_o) dt + \frac{1}{T} \int_{DT}^T (-V_o) dt =$$

$$= \frac{1}{T} (V_d - V_o)(DT) + \frac{1}{T} (-V_o)(T - DT) =$$

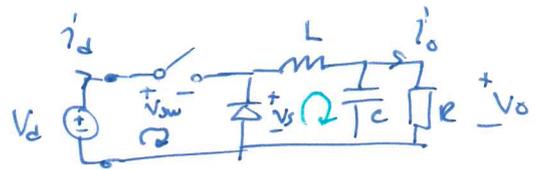
$$= \frac{1}{T} (V_d DT - V_o DT) + \frac{1}{T} (-V_o T + V_o DT) =$$

$$= \frac{1}{T} (V_d DT - V_o DT - V_o T + V_o DT) = V_d D - V_o = 0 \Rightarrow V_o = D V_d$$

• stationärtilstand, ideale komponenter  
• antag - stor C, CCM,

$$P_{in} = P_{out}$$

$$V_d I_d = V_o I_o = D V_d I_o \Rightarrow I_d = D I_o \Rightarrow \underline{\underline{D = \frac{I_d}{I_o}}}$$



KVL  
 $-V_d + V_{sw} + V_s = 0$

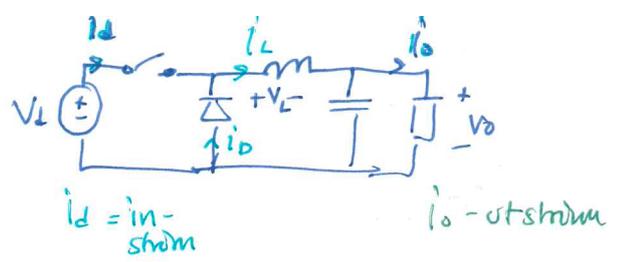
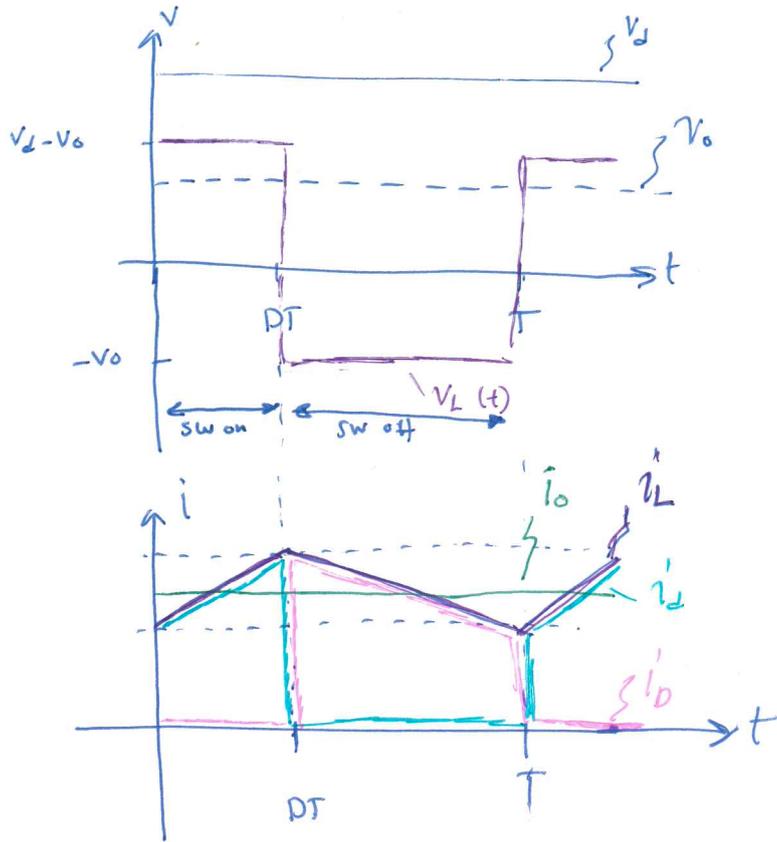
sw on	sw off
$V_{sw} = 0$	$V_s = 0$
$V_d = V_s$	$V_o = V_{sw}$

KVL  
 $-V_s + V_L + V_o = 0$

sw on	sw off
$V_s = V_d$	$V_s = 0$
$V_L = V_d - V_o$	$V_L = -V_o$

$$D = \frac{V_o}{V_d} = \frac{8}{24} = \frac{1}{3}$$

6b)  $v_L, i_o, i_d, i_L, i_p$



$$v_L = L \frac{di_L}{dt}$$

$$v_L > 0 \Rightarrow \frac{di_L}{dt} > 0$$

$$v_L < 0 \Rightarrow \frac{di_L}{dt} < 0$$

6c) CCM om  $\frac{\Delta i_L}{2} < I_{L,ave} = I_o$

$$I_o = \frac{V_o}{R} = \frac{8}{2} = 4 A$$

$$\Delta i_L? \quad v_L = L \frac{di_L}{dt} = L \frac{\Delta i_L}{\Delta t} \Rightarrow \Delta i_L = \frac{v_L \cdot \Delta t}{L} = \int_{\text{on}}^{sw} = \frac{(v_d - v_o)(DT)}{L}$$

$$\Delta i_L = \frac{(v_d - v_o) \cdot D}{f \cdot L} = \frac{(24 - 8) \cdot \frac{8}{24}}{40 \cdot 10^3 \cdot 100 \cdot 10^{-6}} = 1,33 \dots A$$

$$\frac{\Delta i_L}{2} = \frac{2}{3} = 0,666 \dots A < 4 A = I_o \Rightarrow \text{Ja, CCM}$$

7a)  $U_n = 440 \text{ V rms}$   $50 \text{ Hz}$

$T_L = 16 \text{ Nm}$   $n_r = 1210 \text{ rpm}$   $I_{ph} = 3.7 \text{ A}$   $\cos\varphi = 82\%$

i)  $\underline{P_{mek}} = \omega_r \cdot T_e = n_r \cdot \frac{\pi}{20} \cdot T_L = 1210 \cdot \frac{\pi}{30} \cdot 16 = 2027.374459 \text{ W}$

ii)  $P_{f\ddot{u}rd} = P_{in} - P_{ut} = P_{el} - P_{mek}$

$\approx \underline{2027.4 \text{ W}}$

$P_{el} = 3 \cdot V_{ph} \cdot I_{ph} \cdot \cos\varphi = 3 \cdot \frac{440}{\sqrt{3}} \cdot 3.7 \cdot 0.82 = 2312.2185 \text{ W}$

$\underline{P_{f\ddot{u}rd}} = 2312.218546 - 2027.374459 = \underline{284.84 \text{ W}}$

iii)  $\underline{\eta} = \frac{P_{ut}}{P_{in}} = \frac{P_{mek}}{P_{el}} = \frac{2027.374459}{2312.218546} = 0.876809 \dots$   
 $\approx \underline{87.7\%}$

7b)

$P=4$

$U_n = 440 \text{ rms } 60 \text{ Hz}$

 $\Delta$ -kopplad

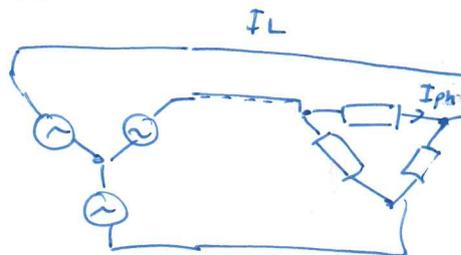
$R_s = 1.1 \Omega$

$R_r' = 0.7 \Omega$

$X_m = 40 \Omega$

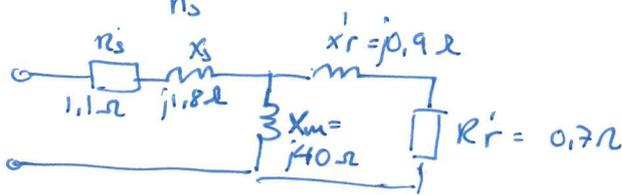
$X_s = 1.8 \Omega$

$X_r' = 0.9 \Omega$



i) i start ögonblicket  $n_r = 0 \Rightarrow s = \frac{n_s - n_r}{n_s} = 1$

$\frac{R_r'}{s} = R_r'$



ii)  $I_L = \sqrt{3} \cdot I_{ph}$  i delta-kopplad last

$$Z_{eq} = R_s + jX_s + \frac{jX_m (R_r' + jX_r')}{jX_m + R_r' + jX_r'} = 1.1 + j1.8 + \frac{j40(0.7 + j0.9)}{j40 + 0.7 + j0.9} =$$

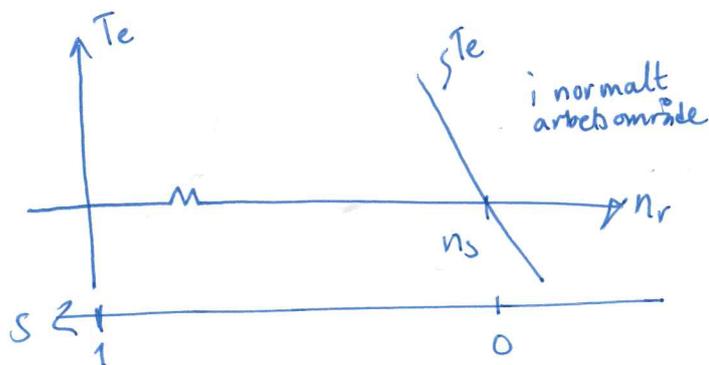
$$= 1.769736043 + j2.691651228 = 3.22110 \angle 56.68139^\circ$$

$$I_{ph} = \frac{U_n}{Z_{eq}} = \frac{440 \angle 0^\circ}{3.22110 \angle 56.68^\circ} = 136.59929 \angle -56.68^\circ \text{ A}$$

$$|I_L| = \sqrt{3} \cdot |I_{ph}| = \sqrt{3} \cdot 136.59929 = \underline{\underline{236.5969251 \dots \text{ A}}}$$

$$f_{rotor} = s \cdot f_{stator} = 1 \cdot 60 = \underline{\underline{60 \text{ Hz}}}$$

7c)



8a)  $\hat{i}_{sd}, \hat{i}_{sq} ?$

$$\beta = 132^\circ$$

$$I_{mag} = ?$$

$$\hat{i}_{sd} = I_{mag} \cdot \cos \beta$$

$$\hat{i}_{sq} = I_{mag} \sin \beta$$

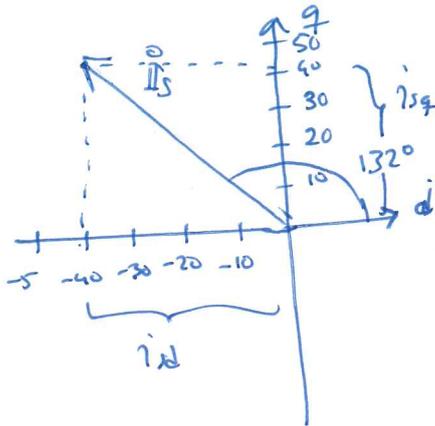
$$P_{cu, \text{ford}} = 3 R_s \cdot I_{rms}^2 = 5.1 \text{ kW}$$

$$\Rightarrow I_{rms} = \sqrt{\frac{P_{cu, \text{ford}}}{3 R_s}} = \sqrt{\frac{5.1 \cdot 10^3}{3 \cdot 0.88}} = 43.95 \text{ A}$$

$$I_{mag} = \sqrt{2} \cdot I_{rms} = \sqrt{2} \cdot 43.95 = 62.16 \text{ A}$$

$$\hat{i}_{sd} = 62.16 \cdot \cos 132^\circ = -41.59 \text{ A}$$

$$\hat{i}_{sq} = 62.16 \cdot \sin 132^\circ = 46.19 \text{ A}$$



8b)  $f_s = ?$

$$n_r = 3400 \text{ rpm} \quad n_p = \frac{4}{2} = 2$$

$$\omega_s = 2\pi f_s \Rightarrow f_s = \frac{\omega_s}{2\pi} = \left\{ \omega_s = \omega_r \right\} = \frac{\omega_r}{2\pi} = \left\{ \omega_r = n_r n_p \right\} = \frac{n_r n_p}{2\pi}$$

$$f_s = \frac{n_r n_p}{2\pi} = \left\{ n_r = n_r \cdot \frac{\pi}{30} \right\} = n_r \cdot \frac{\pi}{30} \cdot \frac{n_p}{2\pi} = \frac{n_r \cdot n_p}{60} = \frac{n_r \cdot 2}{60} = \frac{3400 \cdot 2}{60} =$$

$$\underline{\underline{f_s = 113.33 \dots \text{ Hz}}}$$